

# One-Bit Delta Sigma D/A Conversion

## Part I: Theory

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# 1 What Is A D/A Converter?

- Rick Lyons [1] derives A/D SNR as a function of word length  $N$  and loading factor  $LF$ :

$$\text{SNR} = 6.02N + 4.77 + 20 \log_{10}(LF),$$

- $LF$  is the “loading factor,” a value representing the normalized RMS value of the input signal. For a sine wave,  $LF = 0.707$ . Here we ignore the constant factor of 1.77 dB and we round the  $N$  coefficient to 6 to simplify.
- This can be generalized to express the SNR of any N-bit amplitude-quantized transfer function and thus applies to D/A conversion as well.

For a generic D/A converter in which bandwidth, output bit-width, and other parameters may not be clearly defined, this motivates the following

**Definition 1** *An  $N$ -bit D/A converter converts a stream of discrete-time, linear, PCM samples of  $N$  bits at sample rate  $F_s$  to a continuous-time analog voltage with a signal-to-quantization-noise power ratio of  $6N$  dB in a bandwidth of  $F_s/2$  Hz.*

This gives a basis by which we may evaluate the number of bits of any converter architecture (resistor-ladder, delta-sigma, etc.).

## 2 Delta Sigma Conversion Revealed

- A **delta sigma** D/A converter “transforms” (i.e. requantizes) an  $N$ -bit PCM signal into a 1-bit signal.
- Why requantize to a lower resolution? Because a 1-bit output is extremely easy to implement in hardware and there are ways to make that one-bit output have the SNR of an  $N$ -bit converter.
- How do you get an  $N$ -bit-to-1-bit quantizer, which would normally only produce a  $6 \cdot 1 = 6$  dB SNR, to produce the required  $6N$  dB SNR? *By using **oversampling** and **noise-shaping** to modify the 1-bit output.*

### 3 Oversampling

- Quantization noise is assumed white and uniformly-distributed with a total power of  $q^2/12$ , where  $q$  is the quantization step-size.
- **NOTE: The total quantization noise power does NOT depend on the sample rate!!!**
- Quantization noise modeled as a noise source added to the signal:

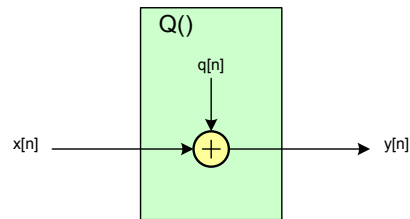


Figure 1: Quantizer Model

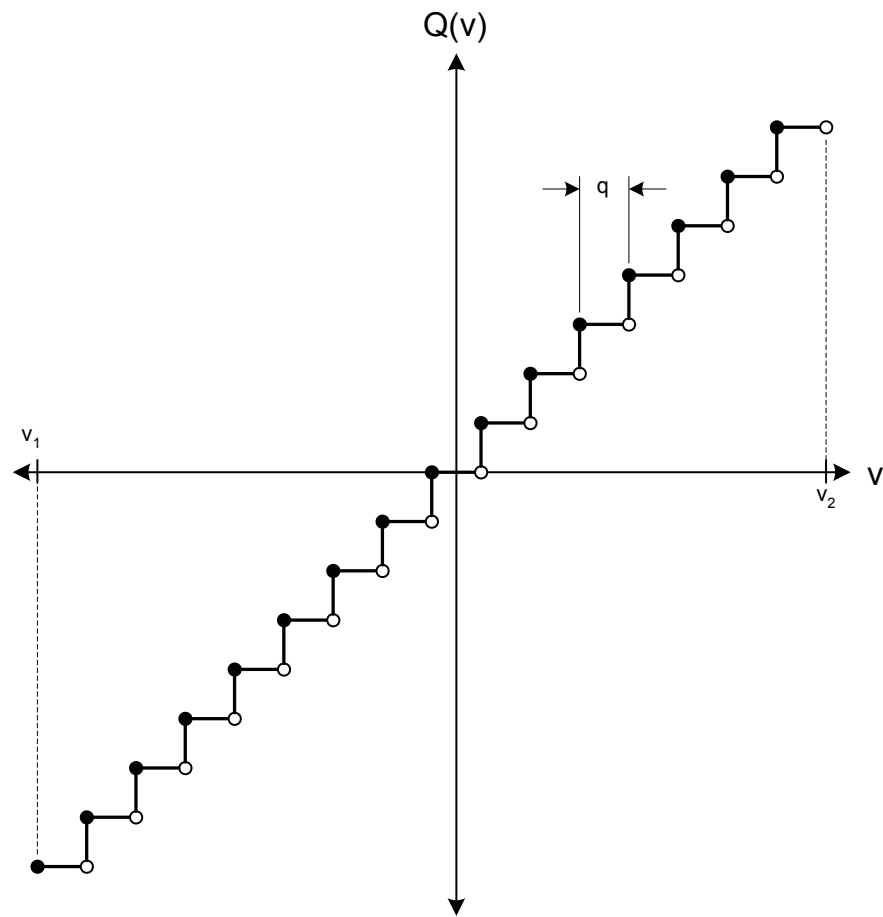


Figure 2: Quantizer Transfer Function

The “in-band” quantization noise power can be reduced by sampling at a rate higher than Nyquist.

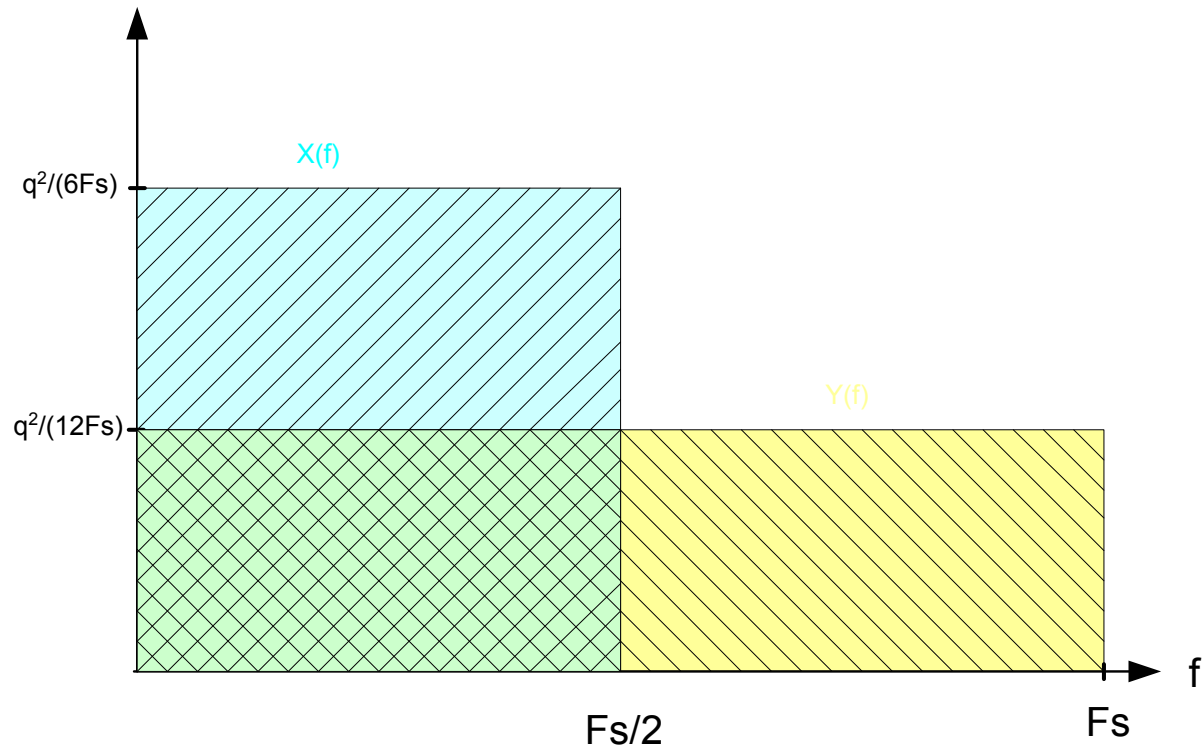


Figure 3:  $2\times$  Oversampled Quantization Noise Spectrum



Since the total in-band noise power is reduced, the number of “effective” bits is increased from the actual bits according to the relationship

$$M = 4^K,$$

where  $M$  is the oversampling factor and  $K$  is the number of extra bits.

Integer oversampling ratios are performed by using an interpolator:

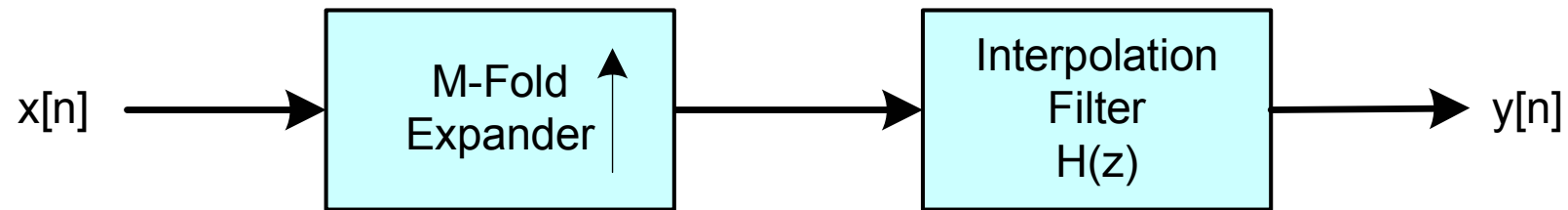


Figure 4: Interpolator Block Diagram

**Oversampling alone is an inefficient way to obtain extra bits of resolution.** A gain of even a few bits would require astronomical oversampling ratios! We must use the additional technique of *noise-shaping* to make a 1-bit converter feasible.

## 4 Noise-Shaping

Shapes the oversampled quantization noise spectrum so that less noise is in-band:

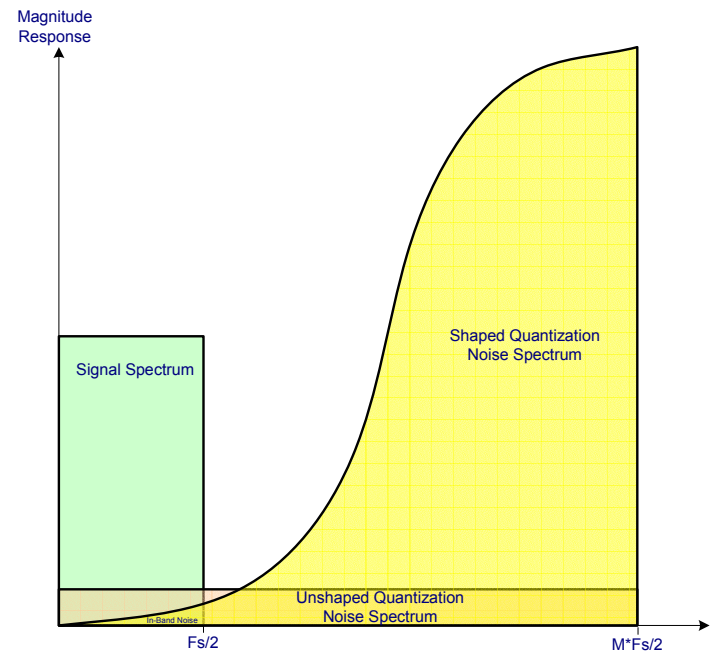


Figure 5: Typical Noise-Shaped Spectrum

Noise-shaping is accomplished by placing feedback around the quantizer:

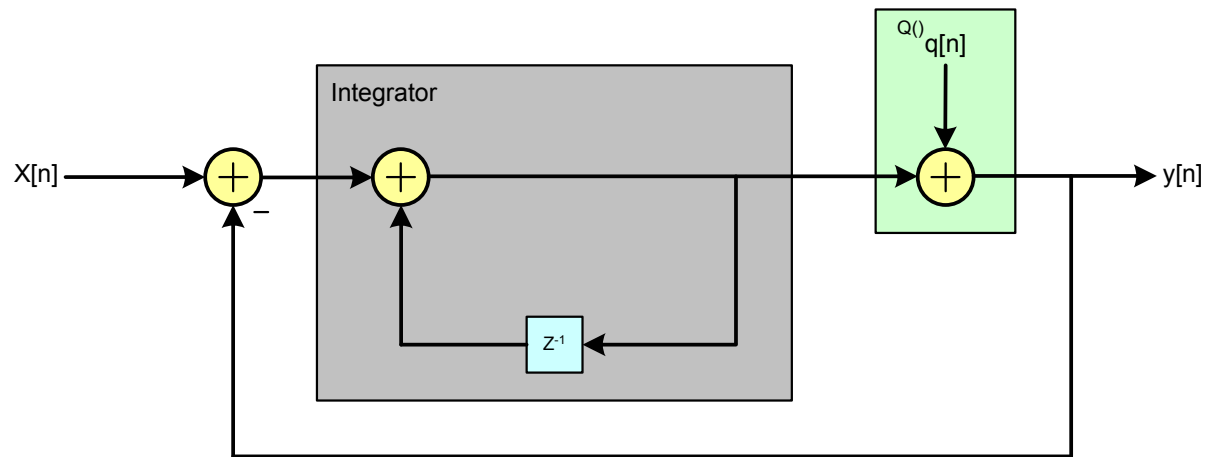


Figure 6: Classic First-Order Noise-Shaper

The transfer function of figure 6 is derived as follows:

$$\begin{aligned}
 W(z) &= X(z) - z^{-1}Y(z) \\
 \Sigma(z) &= W(z) + z^{-1}\Sigma(z) \implies \Sigma(z) = \frac{W(z)}{1 - z^{-1}} \\
 Y(z) &= \Sigma(z) + Q(z) = \frac{W(z)}{1 - z^{-1}} + Q(z) \\
 (1 - z^{-1})Y(z) &= W(z) + (1 - z^{-1})Q(z) \\
 &= X(z) - z^{-1}Y(z) + (1 - z^{-1})Q(z) \\
 Y(z) &= X(z) + (1 - z^{-1})Q(z) \tag{1}
 \end{aligned}$$

It is clear from equation 1 that the signal  $X(z)$  passes through unmodified while the quantization noise  $Q(z)$  is modified by the term  $1 - z^{-1}$ . In delta-sigma modulator terminology this quantization noise coefficient is referred to as the *noise transfer function* [2], or NTF, denoted  $N(z)$ . Thus  $N(z) = 1 - z^{-1}$ .

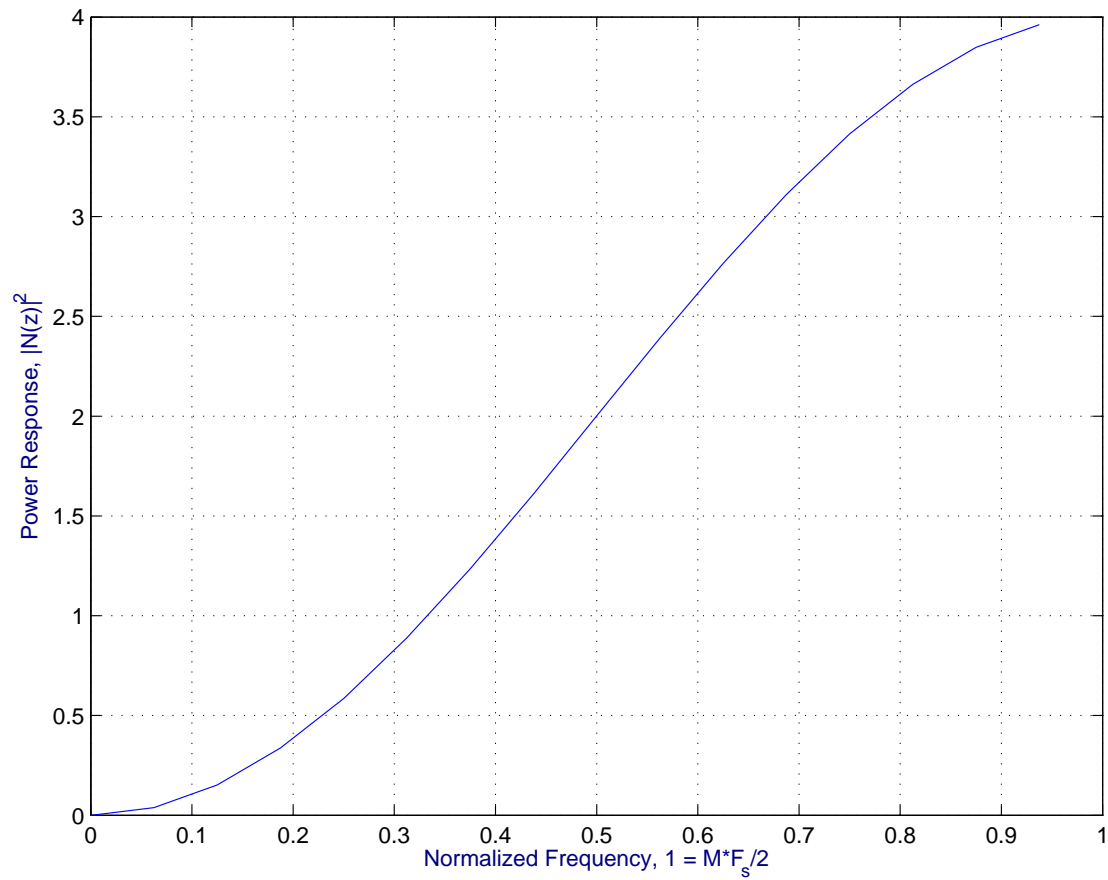


Figure 7: Noise Transfer Function Power Response of a First-Order Modulator

The noise-shaping can be made stronger by embedding integrator loops:

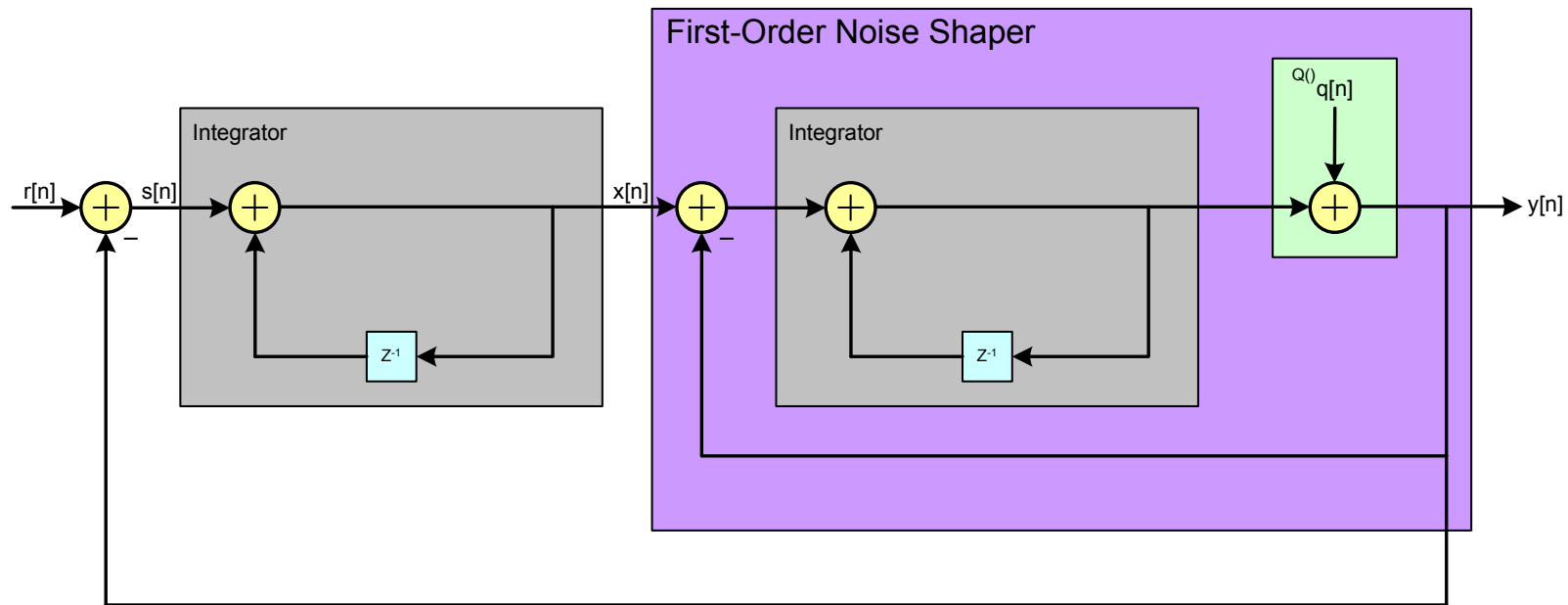


Figure 8: Second-Order Delta-Sigma Modulator



- The number of embeddings is termed the *order* of the modulator. An  $L$ th-order modulator has NTF

$$N(z) = (1 - z^{-1})^L.$$

- It can be shown [3] that the in-band quantization noise power relative to the maximum signal power as a function of oversampling ratio  $M$  and modulator order  $L$  is

$$\frac{6L + 3}{2\pi^{2L}} M^{2L+1}.$$

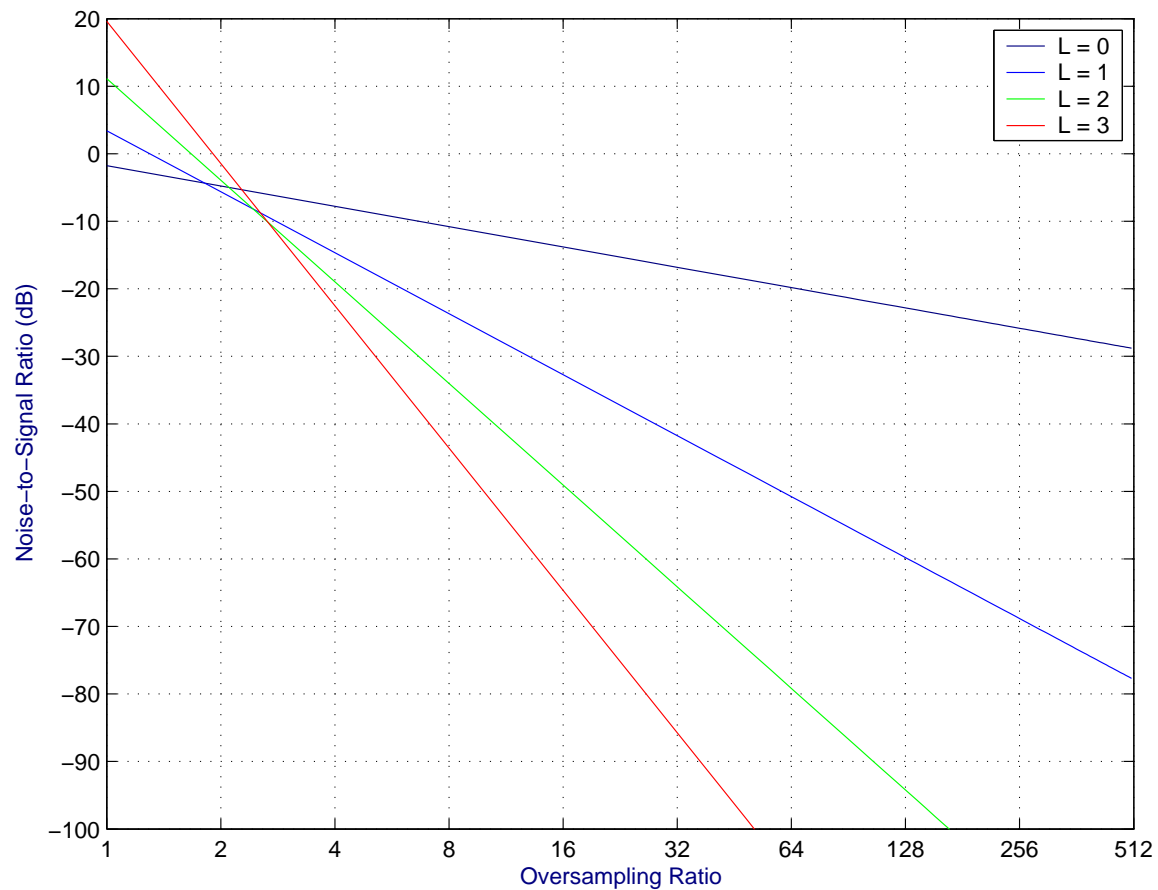


Figure 9: Ratio of In-Band Quantization Noise Power To Signal Power versus Oversampling Ratio and Modulator Order  $L$

## 5 Alternate Modulator Architecture

$$Y(z) = X(z) + (1 - z^{-1}H(z))Q(z). \quad (2)$$

To be equivalent with the classic architecture,  $H(z) = z - zG(z)$ . Is  $H(z)$  realizable???

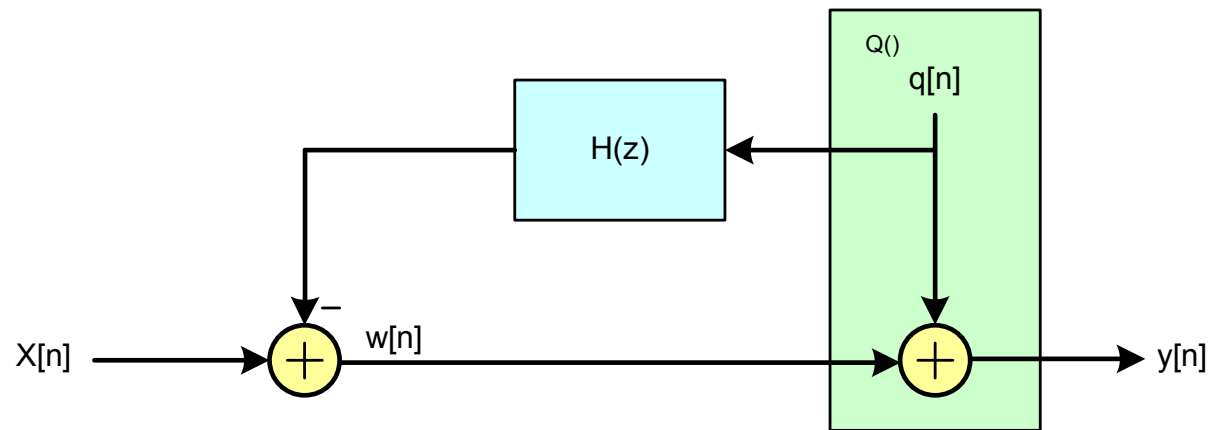


Figure 10: Alternate Delta-Sigma Modulator Architecture

Add dither to get rid of “birdies:”

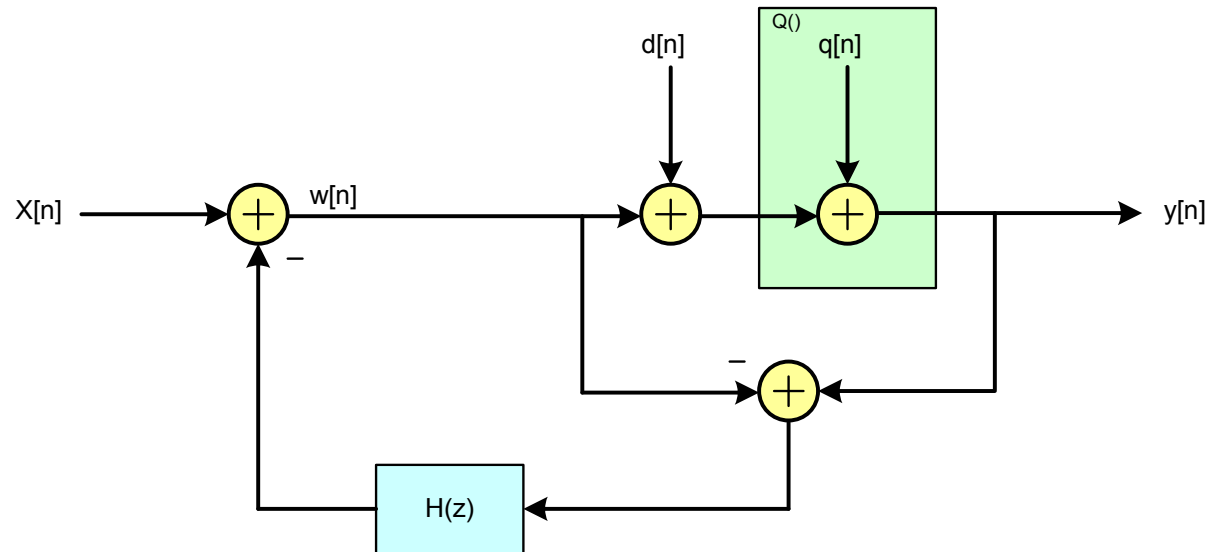


Figure 11: Delta Sigma Modulator with Dither

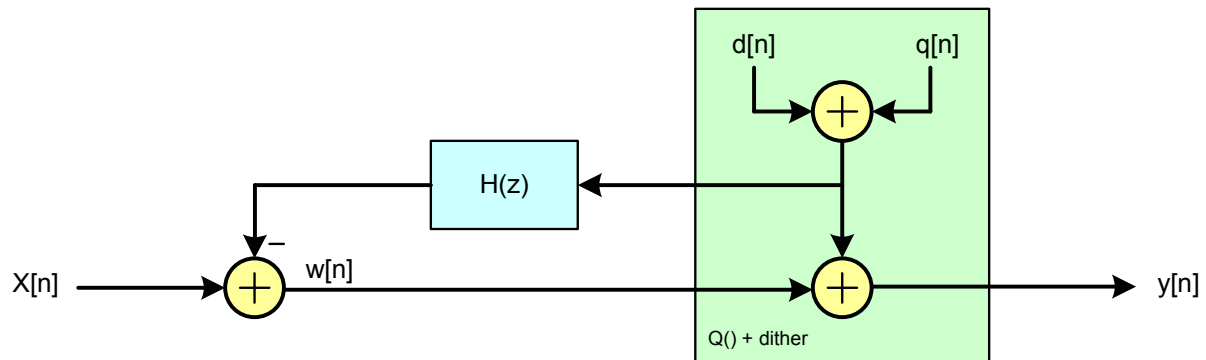


Figure 12: Equivalent Dithered Modulator

## 6 Psychoacoustic Noise-Shaping

- The alternate architecture admits any NTF of the form

$$N(z) = 1 - z^{-1}H(z).$$

- The classic  $L$ th-order modulator NTF contains  $L$  zeros at  $z = 1$  (DC),

$$N(z) = \frac{(z - 1)^L}{z^L}.$$

- When  $L$  is even we can use conjugate pairs to place the zeros at any  $L/2$  frequencies on the unit circle.

Example: For  $L = 2$ , we can place the zero at any frequency  $f$ ,  $0 \leq f \leq MF_s/2$ :

$$N(z) = \frac{z^2 - 2 \cos\left(\pi \frac{f}{MF_s}\right) + 1}{z^2}.$$

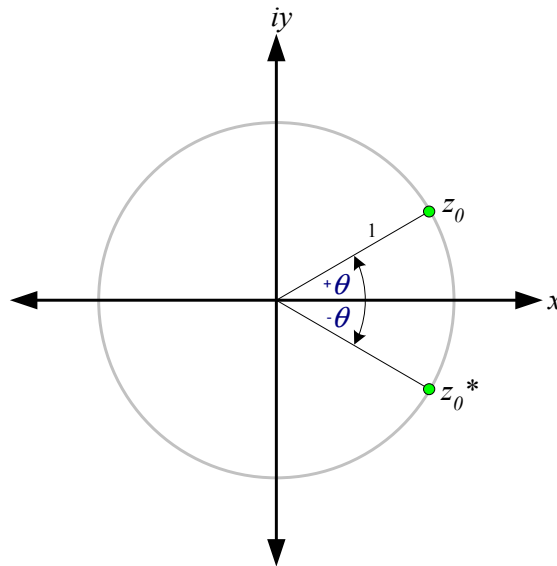


Figure 13: Zeros for Psychoacoustic Noise-Shaping,  $\theta = \pi \frac{f}{MF_s}$ .

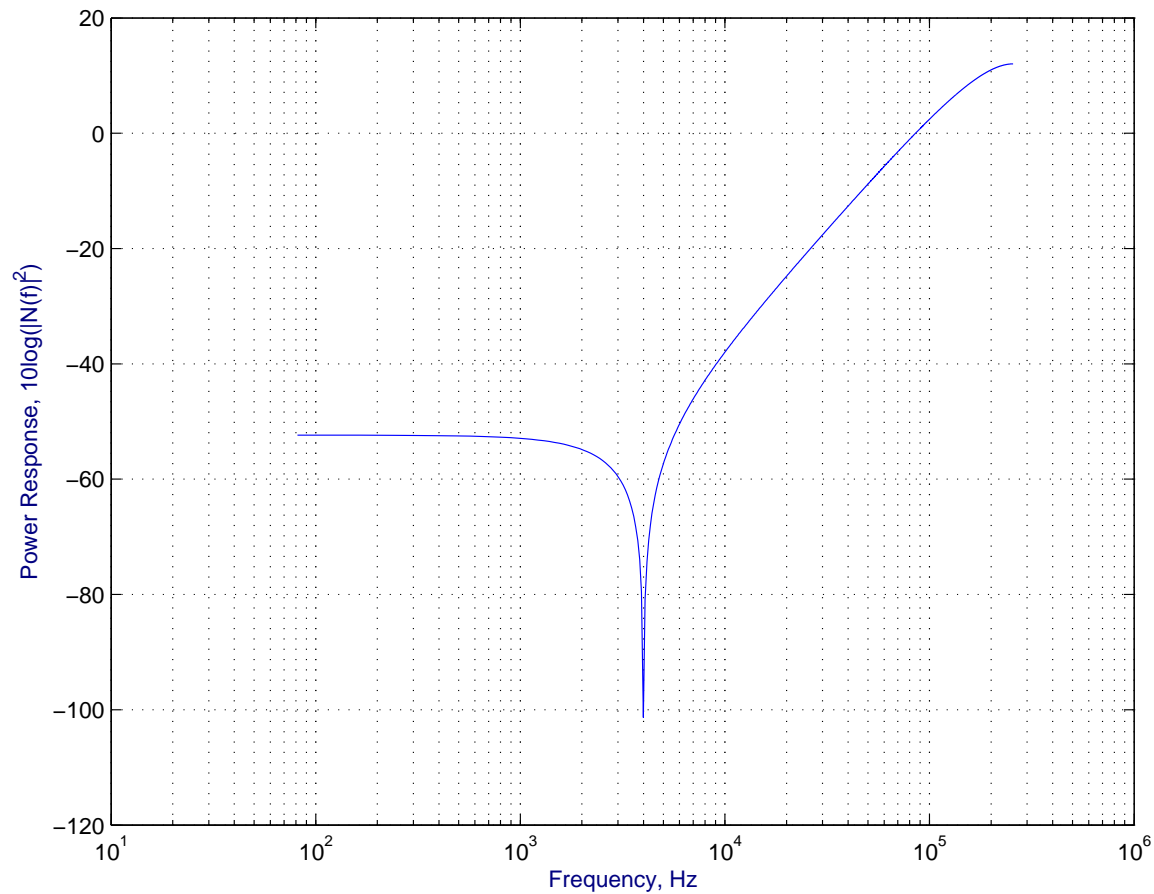


Figure 14: NTF Power Response  $|N(f)|^2$  of Psychoacoustically Noise-Shaped Modulator with  $f = 4$  kHz



## 7 The Complete Modulator

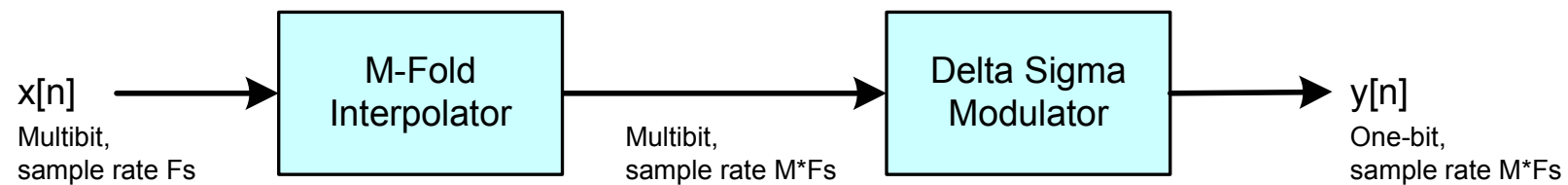


Figure 15: Delta Sigma D/A Converter Block Diagram

## 8 References

### References

- [1] Richard G. Lyons. *Understanding Digital Signal Processing*. Prentice Hall, second edition, 2004.
- [2] Steven R. Norsworthy, Richard Schreier, and Gabor C. Temes. *Delta-Sigma Data Converters: Theory, Design, and Simulation*. IEEE Press, 1997.
- [3] David Johns and Ken Martin. *Analog Integrated Circuit Design*. Wiley Publishers, 1997.